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# Equazione Radar e filtro adattato

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# Matched filtering (I)

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- If the radar transmission is coherent, it is possible to transmit a long duration pulse (with the advantage of reduced peak power) and compress the echoes received to resemble the echoes from a very short pulse (with the advantages of good range resolution).

$$\underline{|S(\tau)|^2}$$

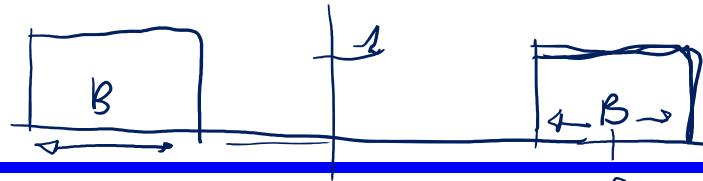
## Matched filter characteristics

- 1) A matched filter gives the best possible Signal/Noise power ratio (S/N) at Receiver output.  
This S/N ratio is proportional to the energy contained in the signal waveform.
- 2) A receiver can be matched to a transmitted waveform by making its impulse response the time reverse of that waveform.  
ie.  $y(t)_{\text{FILTER}} = s^*(-t)_{\text{SIGNAL}}$  it follows that:  $Y(\omega)_{\text{FILTER}} = S^*(\omega)_{\text{SIGNAL}}$   
(Receiver frequency response is complex conjugate of transmit signal spectrum)
- 3) The output waveform of a matched filter receiver is the delayed autocorrelation of the transmitted signal waveform.

## Sistemi Radar

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# Matched filtering (II)



$s(t)$  Input signal  
 $y(t)$  Output signal

$h(t)$  Impulse response  
 $t_1$  time of maximum

Signal output power at time  $t_1$

$$\rightarrow P_{S_{out}} = |y(t_1)|^2 = \left| \int_{-\infty}^{+\infty} Y(f) e^{j2\pi f t_1} df \right|^2 = \left| \int_{-\infty}^{+\infty} S(f) H(f) e^{j2\pi f t_1} df \right|^2$$

Noise output power

$$\rightarrow N_{out} = \int_{-\infty}^{+\infty} N(f) |H(f)|^2 df = \left( \frac{N_0}{2} \right) \int_{-\infty}^{+\infty} |H(f)|^2 df$$

With noise power spectral density  $N(f)$

$$P_n = \left( \frac{K T_0}{2} \right) \cdot 2(B_n)$$

# Matched filtering (III)

$$\frac{S}{N}_{out} = \frac{1}{2} \frac{\left| \int_{-\infty}^{+\infty} S(f) H(f) e^{j2\pi f t_1} df \right|^2}{\int_{-\infty}^{+\infty} N(f) |H(f)|^2 df}$$

$$N(f) = \frac{N_0}{2}$$

$$\frac{S}{N}_{out} = \frac{2 \left| \int_{-\infty}^{+\infty} S(f) H(f) e^{j2\pi f t_1} df \right|^2}{N_0 \int_{-\infty}^{+\infty} |H(f)|^2 df}$$

$\left| \int f \circ g dt \right|^2 \leq \int |f|^2 dt \cdot \int |g|^2 dt$

Schwartz inequality:

$$\frac{S}{N}_{out} \leq \frac{\sqrt{\int_{-\infty}^{+\infty} |S(f)|^2 df} \sqrt{\int_{-\infty}^{+\infty} |H(f)|^2 df}}{N_0 \int_{-\infty}^{+\infty} |H(f)|^2 df} = \frac{E}{N_0}$$

$$\left| \int f \circ g dt \right|^2 = \int |f|^2 dt \cdot \int |g|^2 dt$$

$$f = g^*$$

# Matched filtering (IV)

$$\frac{S}{N}_{out} = \frac{\left| \int_{-\infty}^{+\infty} S(f) H(f) e^{j2\pi f t_1} df \right|^2}{N_0 \int_{-\infty}^{+\infty} |H(f)|^2 df} = \frac{E}{N_0}$$

Obtained for

$$H(f) = G \cdot S^*(f) e^{-j2\pi f t_1}$$

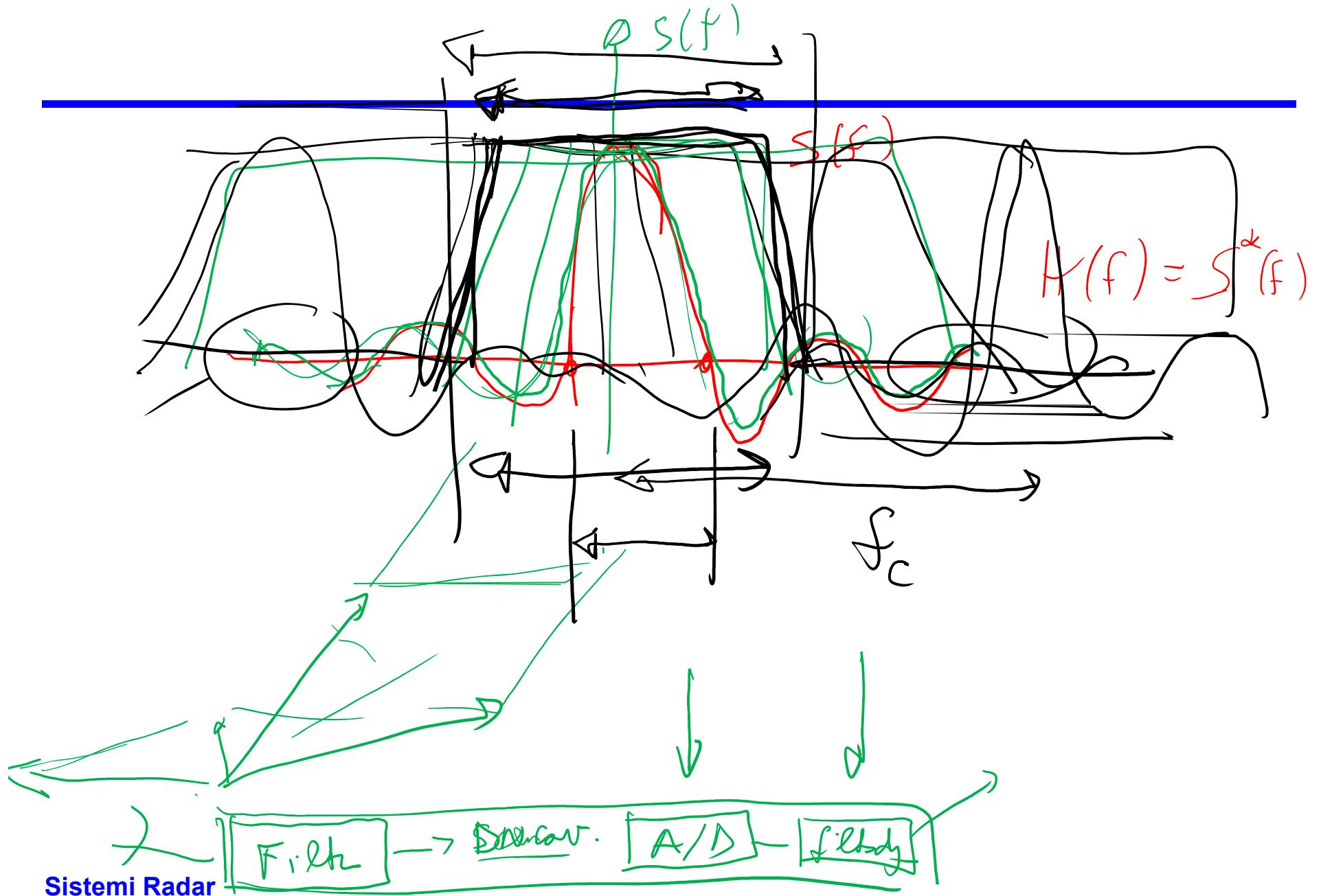
$$h(t) = G \cdot s^*(t_1 - t)$$

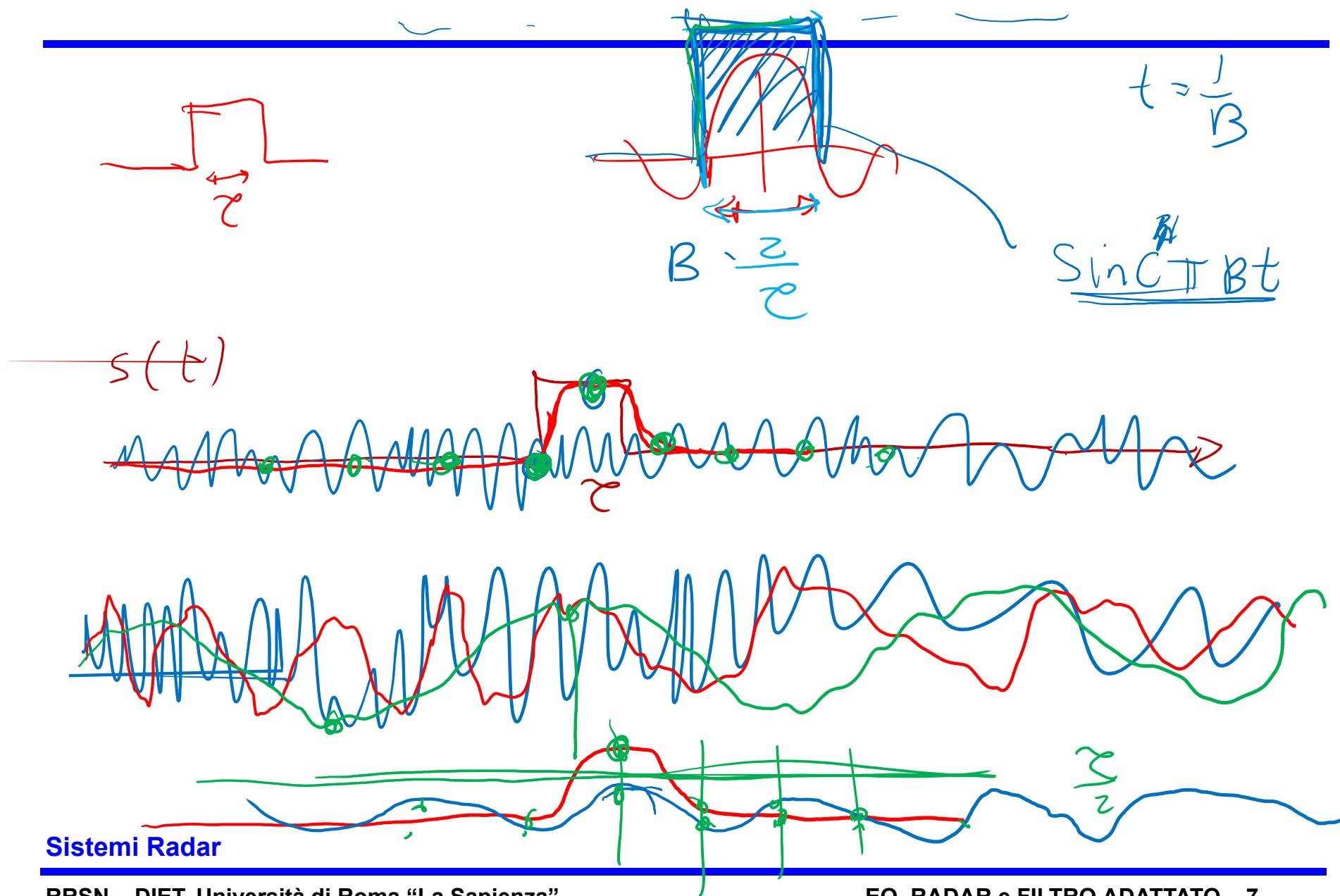
$$N_{out} = N_0 \int_{-\infty}^{+\infty} |H(f)|^2 df = G^2 N_0 \int_{-\infty}^{+\infty} |S(f)|^2 df = G^2 E_s N_0$$

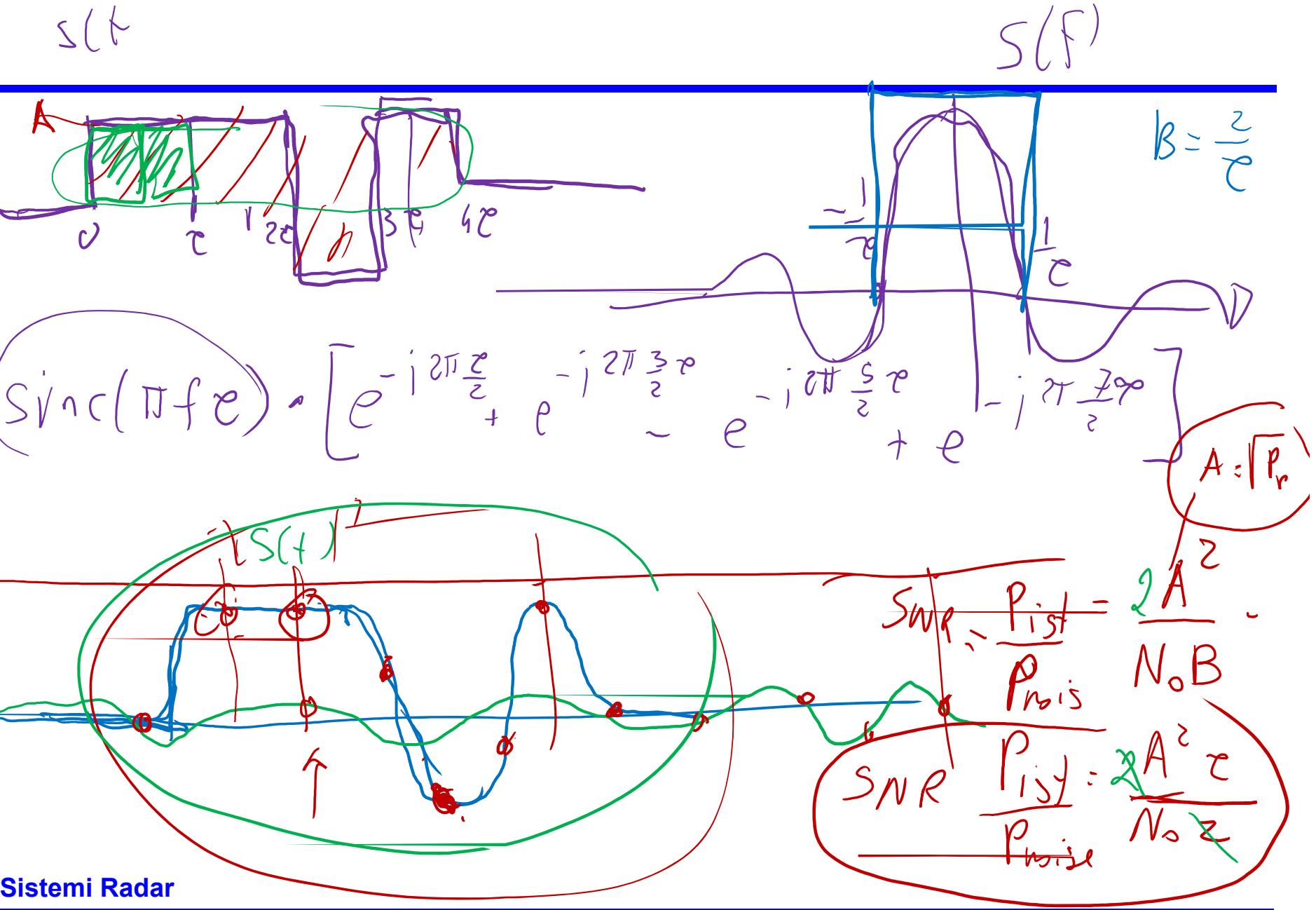
$$|y(t_1)|^2 = \left| \int_{-\infty}^{+\infty} S(f) H(f) e^{j2\pi f t_1} df \right|^2 = G^2 \left| \int_{-\infty}^{+\infty} |S(f)|^2 df \right|^2 = G^2 |E_s|^2$$

To maintain output noise power level equal to input use  
 - especially important in digital matched filter implementation to use bit dynamics

$$G^2 E_s = 1 \Rightarrow G = \sqrt{E_s}$$









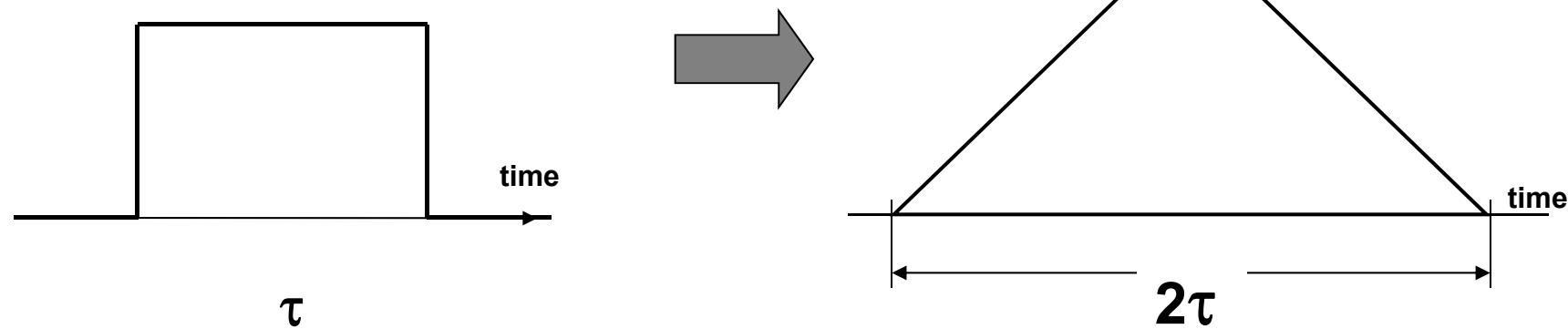




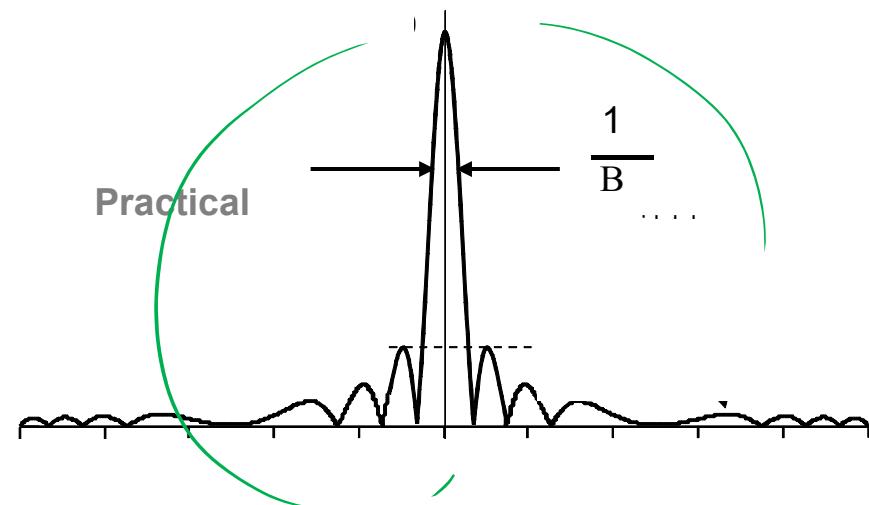
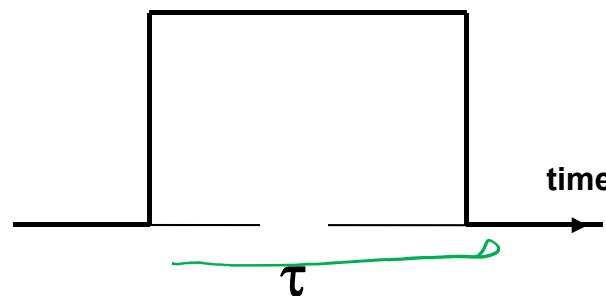
# Matched filtering (V)

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Non-modulated Rectangular pulse:



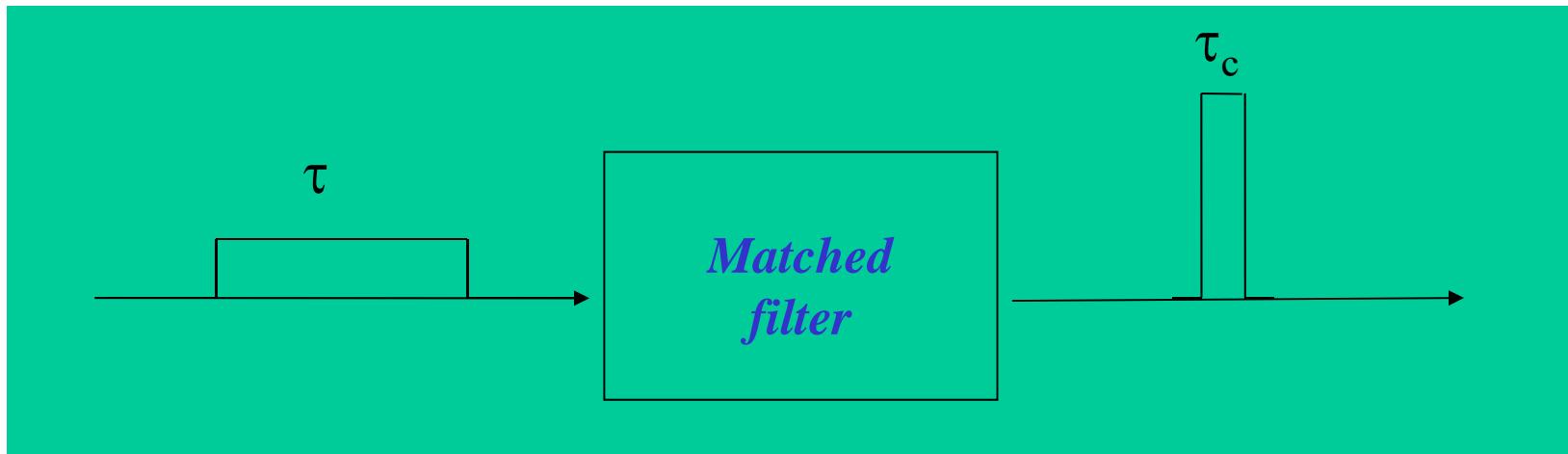
Phase-modulated rectangular pulse:  
With overall bandwidth B



# Matched filtering (VI)

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- We want to transmit a long pulse (length  $\tau$ ) to get energy on target
- But we want a short compressed output (length  $\tau_c \approx 1/B$ ) and larger amplitude:



Passive Filter  $\longrightarrow$  principle of energy conservation:

$$E_o = E_i \quad \longrightarrow$$

$$P_{po} \tau_c = P_{pi} \tau$$

# Matched filtering (VII)

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Passive Filter

principle of energy conservation:

$$E_o = E_i \quad \longrightarrow \quad P_{po} \tau_c = P_{pi} \tau$$

$$P_{po} = P_{pi} \quad \tau / \tau_c = P_{pi} / B\tau$$

Noise power level does not change

**Signal power improved with respect to noise power of**

$$\tau / \tau_c = P_{pi} / B\tau$$

**COMPRESSION RATIO**

# Equazione Radar con compressione

## Varie forme dell'Equazione Radar

L'equazione radar, e di conseguenza l'espressione della portata, può essere particolarizzata in dipendenza delle applicazioni

$$\left(\frac{S}{N}\right)_r = \frac{P_r}{P_n} = \frac{P_t G A_e \sigma}{(4\pi R^2)^2 k T_0 B F L} B \tau = \frac{P_t G A_e \sigma \tau}{(4\pi R^2)^2 k T_0 F L}$$

- 1 Si suppone di aver fissato il massimo valore del guadagno d'antenna  $G$  (vincolo la larghezza del fascio e quindi la risoluzione angolare): utilizzando  $G=4\pi A_e / \lambda^2$

$$\left(\frac{S}{N}\right)_r = \frac{P_t G^2 \lambda^2 \sigma \tau}{(4\pi)^3 R^4 k T_0 F L} \rightarrow R_{\max} = \left[ \frac{P_t G^2 \lambda^2 \sigma \tau}{(4\pi)^3 k T_0 B F L (S/N)_{\min}} \right]^{1/4}$$

Preferibili le basse frequenze

- 2 Si suppone di aver fissato il massimo valore dell'area geometrica e quindi efficace d'antenna  $A_e$ : utilizzando  $A_e = \lambda^2 G / 4\pi$

$$\left(\frac{S}{N}\right)_r = \frac{P_t A_e^2 \sigma \tau}{4\pi R^4 \lambda^2 k T_0 F L} \rightarrow R_{\max} = \left[ \frac{P_t A_e^2 \sigma \tau}{4\pi \lambda^2 k T_0 F L (S/N)_{\min}} \right]^{1/4}$$

Preferibili le alte frequenze

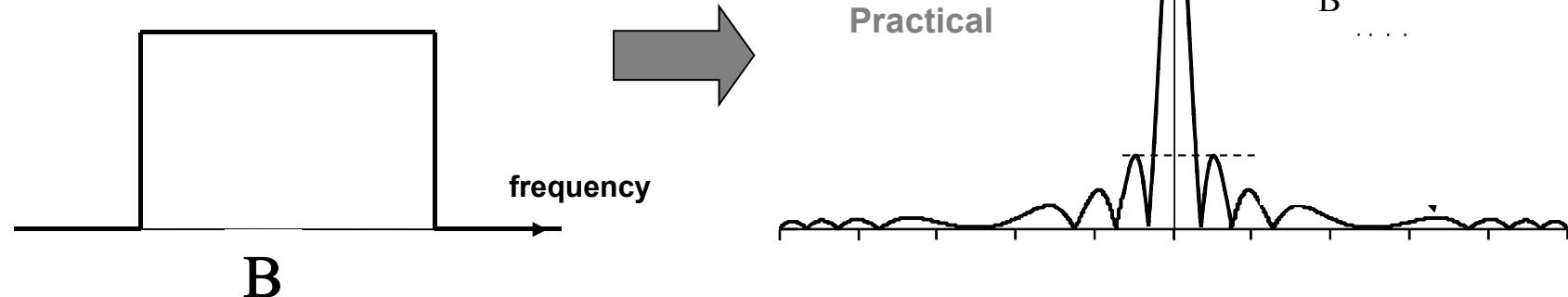
## Sistemi Radar

# Pulse compression yields Sidelobes

Output is signal autocorrelation:

$$|y(t)|^2 = \left| \int_{-\infty}^{+\infty} S(f) H(f) e^{j2\pi f t} df \right|^2 = G^2 \left| \int_{-\infty}^{+\infty} |S(f)|^2 e^{j2\pi f(t-t_1)} df \right|^2 = G^2 |R_{ss}(t-t_1)|^2$$

Approximately fully occupied spectrum  
with overall bandwidth B



E' necessario un controllo dei lobi laterali: pesatura?

$$\delta(t) = \text{rect}_{\frac{T}{2}}(t)$$

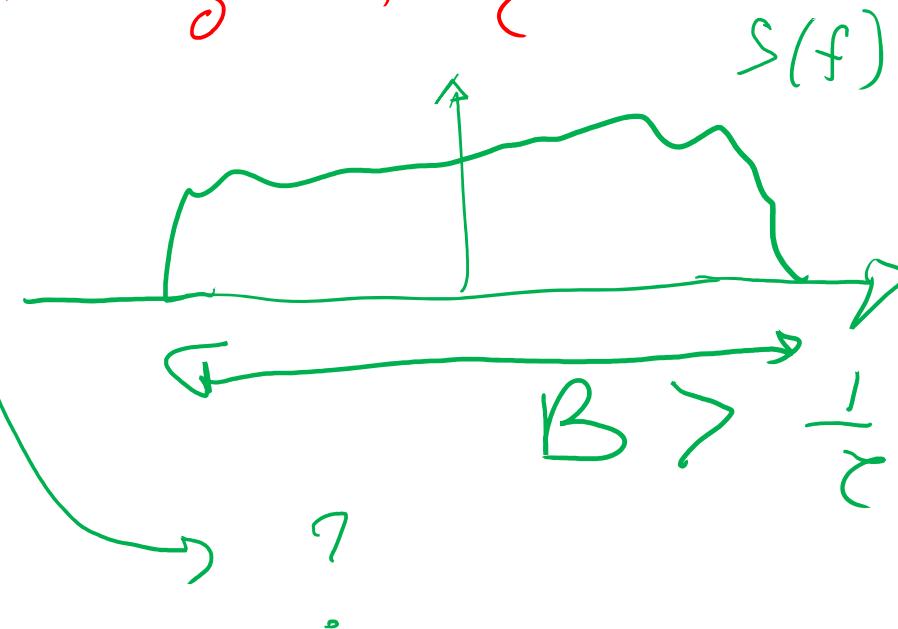
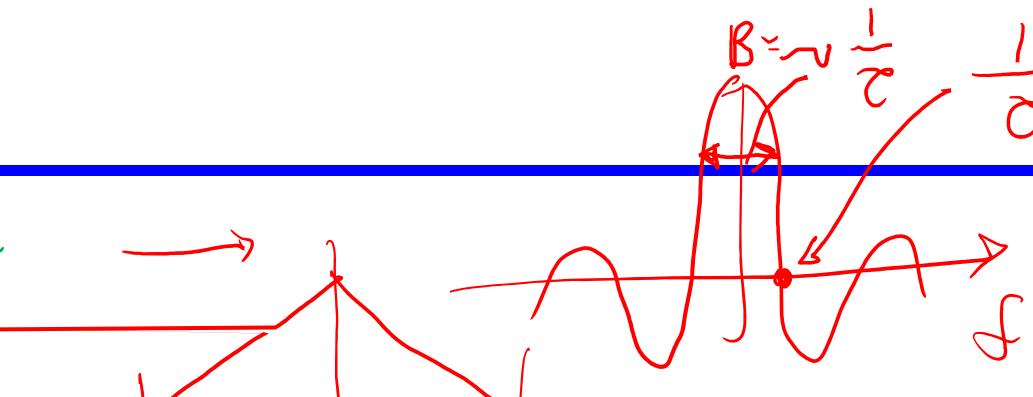
$$A \xrightarrow{\quad} E = A^2 c$$

FA

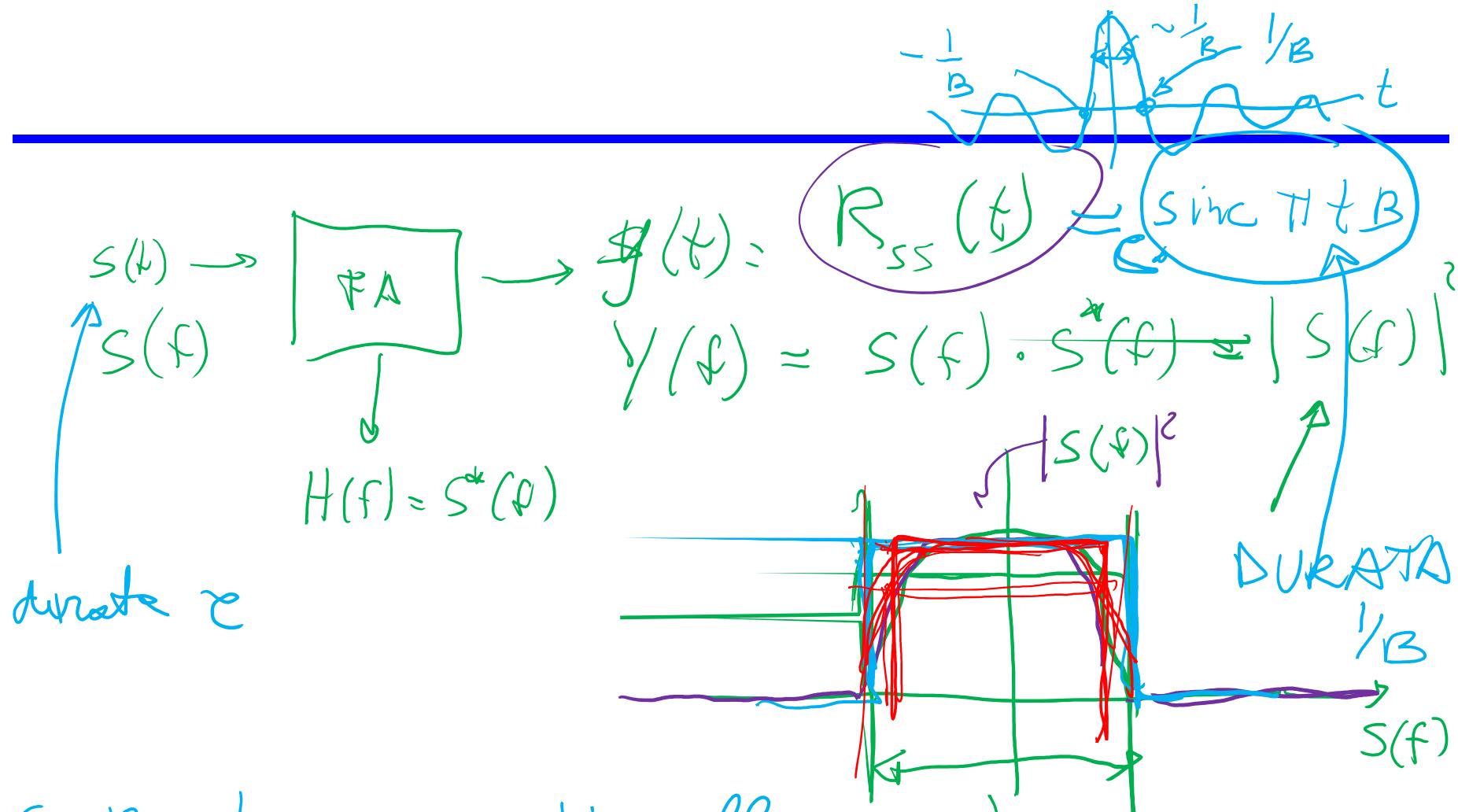
$$S(t) = \text{rect}_{\frac{T}{2}}(t) e^{j\phi(t)}$$

$$|S(t)| = A$$

$$E \approx |S(t)|^2 \cdot c$$



## Sistemi Radar



Se  $B = \frac{1}{\tau}$  non cambia nello (impuls rect)

Se  $B > \frac{1}{\tau}$  ~~compressione~~ =  $\frac{\tau}{1/B} = \cancel{\tau B} \gg 1$   
 Sistemi Radar

$\frac{c}{2} \tau$  (blue oval)       $\frac{1}{B} = 1 \mu s$  (blue oval)       $P_t \cdot \tau = 87 \cdot 10^3 \text{ W}^6$  (red oval)

Ris 150 m (red oval)       $c \approx 1 \mu s$  (blue oval)       $P_t = 87 \text{ kW}$  (red oval)

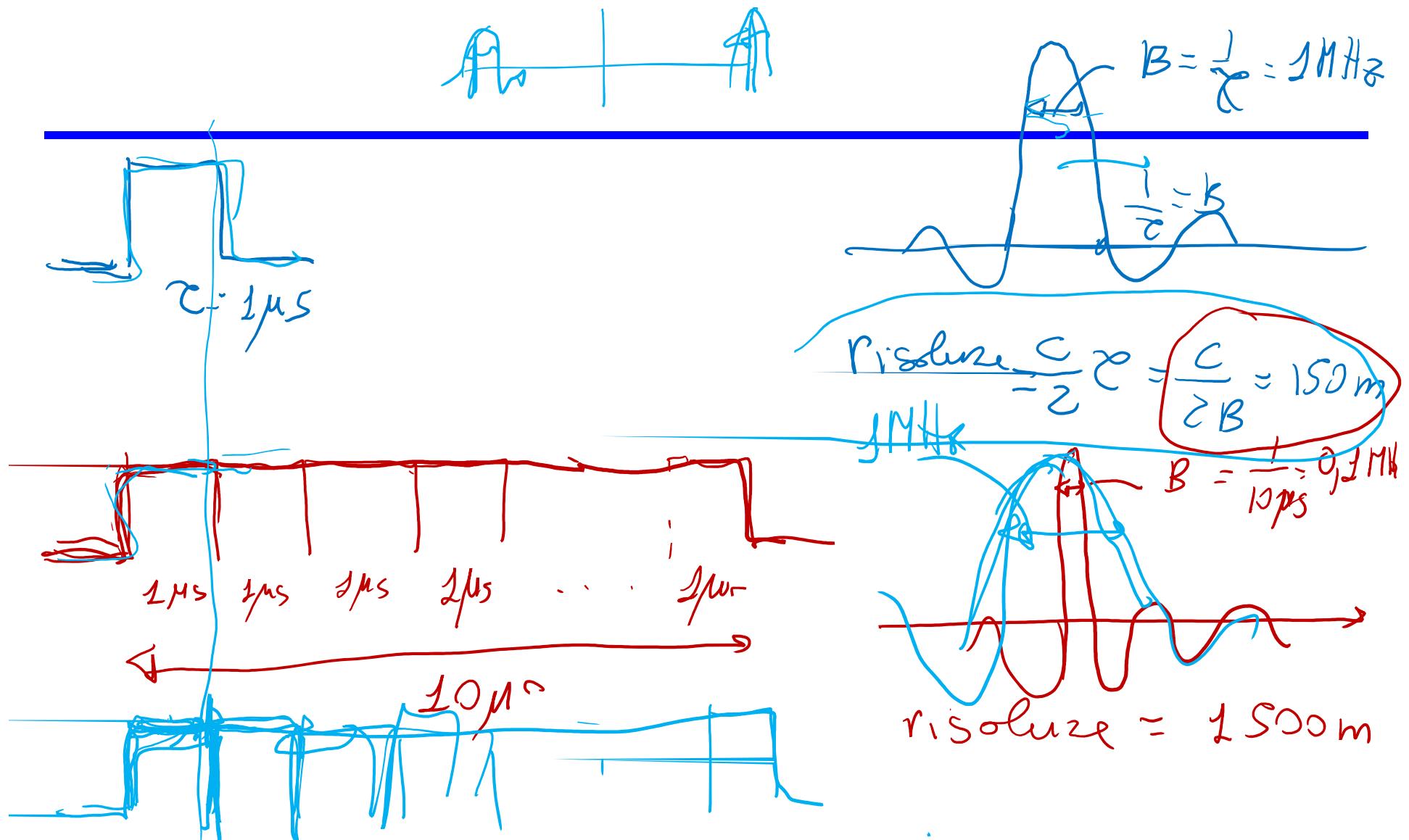
150 km con imp rect       $\tau \rightarrow 100 \mu s$  (red oval)       $\div 100$       870 W

dopo compressione      Ris in dists =  $\frac{c}{2} \cdot \frac{1}{B} = 150 \text{ m}$  (red oval)

$c = \frac{1}{1M\mu s} = 1 \mu s$  (blue oval)

$\frac{c}{2B} = 150 \text{ m} \rightarrow B = \frac{3 \cdot 10^8}{2 \cdot 150 \text{ m}} \text{ m/s} = 10^6 \text{ 1/s} = 1 \text{ MHz}$  (blue oval)

**Sistemi Radar**



## Sistemi Radar