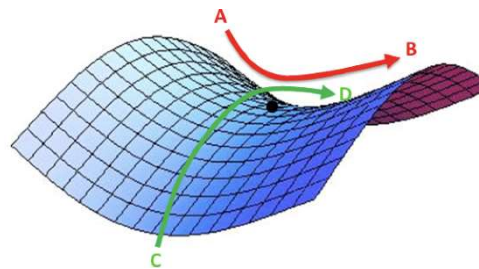


Ph.D. Course on
Analytical Techniques for Wave Phenomena



Lesson 9

Paolo Burghignoli



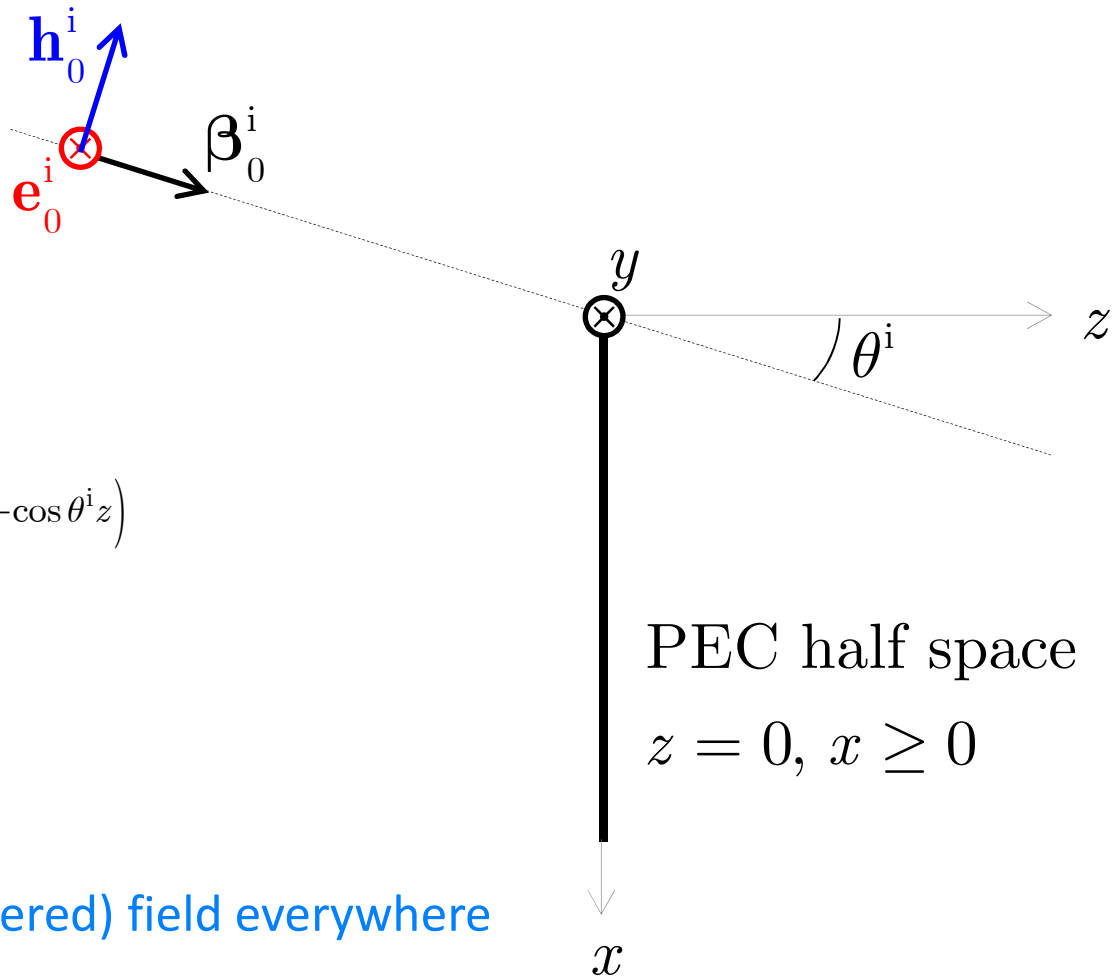
SAPIENZA
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The Sommerfeld Half-Plane Problem: Generalities

The Sommerfeld Half-Plane Problem

A uniform plane wave impinges normally on a PEC half plane with the electric field parallel to its rim:



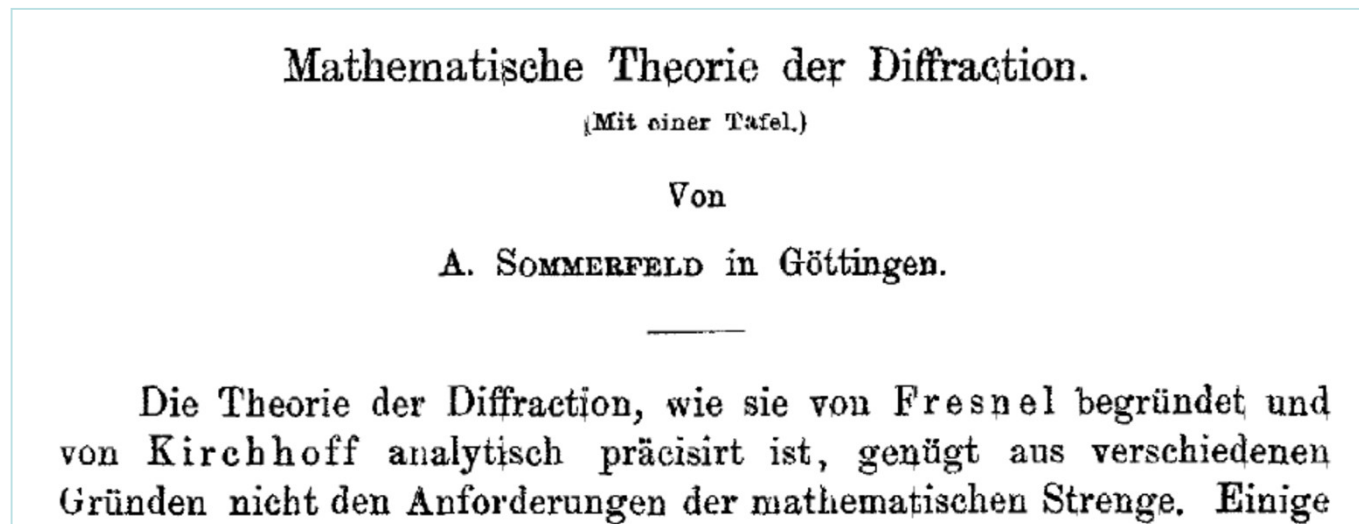
$$\begin{aligned}\mathbf{E}^i &= E_0^i \mathbf{e}_0^i e^{-jk_0 \boldsymbol{\beta}_0^i \cdot \mathbf{r}} \\ &= E_0^i \mathbf{y}_0 e^{-jk_0 (\sin \theta^i x + \cos \theta^i z)}\end{aligned}$$

Problem:

find the total (incident + scattered) field everywhere

Some History

- **A. Sommerfeld** provided the exact solution to the problem of plane-wave diffraction by a PEC half plane in 1896.



[A. Sommerfeld, "Mathematische theorie der diffraction," *Math. Ann.*, vol. 47, no. 2, pp. 317–374, 1896.]

Such a solution, although obtained with an elaborate approach not amenable to be used in different problems, was historically important as it was *the first exact solution* to a diffraction problem.

Some History

- It was realized in the 1940s that the powerful **Wiener-Hopf approach** could be used to solve the problem.

[E. T. Copson, "On an integral equation arising in the theory of diffraction," *Quart. J. Math.*, vol. 17, pp. 19-34, 1946.]

[J. F. Carlson and A. E. Heins, "The reflection of an electromagnetic plane wave by an infinite set of plates," *Quart. Appl. Math.*, vol. 4, pp. 313-329, 1947.]

- In 1951 P. C. Clemmow proposed an alternative approach (based on **dual integral equations**) that works directly with the spectra of the field quantities.

[P. C. Clemmow, "A method for the exact solution of a class of two-dimensional diffraction problems," *Proc. Roy. Soc. London, Ser. A*, vol. 205, pp. 286-308, 1951.]

The Wiener-Hopf/dual-integral-equation method employ crucially *complex analysis* and can be used to solve many different diffraction problems (e.g., half planes and junctions with impedance boundary or transition conditions).

Some History

- Much later, in 1983, F. Gori found that an **elementary solution** to the Sommerfeld half-plane problem could be obtained by employing *cylindrical functions of half-integer order*.



[F. Gori, "Diffraction from a half plane. A new derivation of the Sommerfeld solution," *Optics Commun.*, vol. 48, no. 2, pp. 67–70, Nov. 1983.]

This elementary solution will be illustrated first, after discussing some generalities in the next slides.

Translational Invariance and TM Polarization

- The PEC half plane is **translationally invariant** w.r.t. the y direction
- The incident field is **independent** of the y coordinate and TM^y

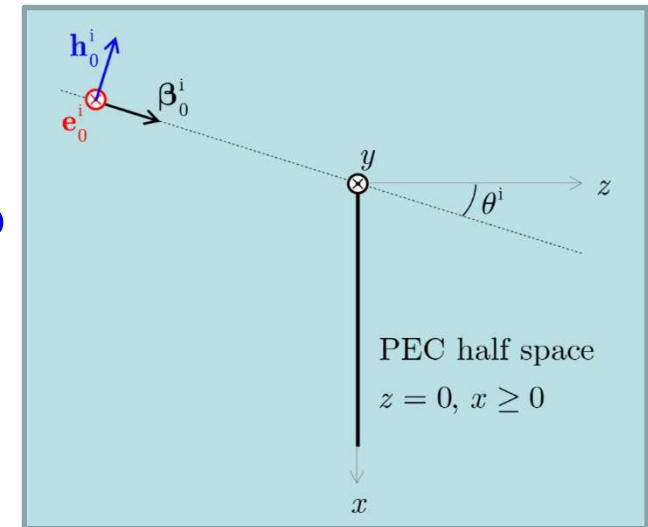


- The scattered (and hence the total) field is also independent of the y coordinate and TM^y
- The only nonzero components of the fields are

$$E_y, H_x, H_z$$

- From the Maxwell equations we may express the magnetic field in terms of the electric field as

$$H_x = \frac{1}{j\omega\mu_0} \frac{\partial E_y}{\partial z}, \quad H_z = -\frac{1}{j\omega\mu_0} \frac{\partial E_y}{\partial x}$$

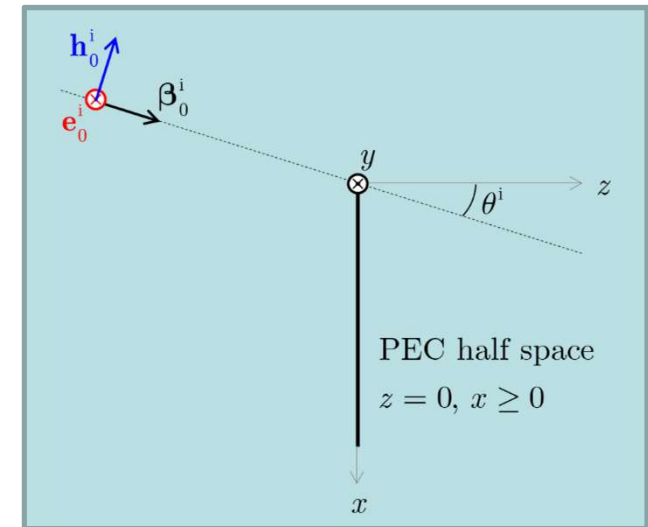


Electric Current Density on the PEC Half Plane

$$\mathbf{J}_s = \mathbf{z}_0 \times [\mathbf{H}]_{-}^{+} = \mathbf{z}_0 \times [\mathbf{x}_0 H_x + \mathbf{z}_0 H_z]_{-}^{+} = \mathbf{y}_0 [H_x]_{-}^{+}$$

$$= \mathbf{y}_0 \frac{1}{j\omega\mu_0} \left[\frac{\partial E_y}{\partial z} \right]_{-}^{+} = \mathbf{y}_0 \frac{1}{j\omega\mu_0} \left[\frac{\partial E_y^s}{\partial z} \right]_{-}^{+}$$

the incident field and its derivatives are continuous in the entire space



The normal derivative of the scattered electric field is **discontinuous** across the PEC half plane.

Such a discontinuity is related to the existence of an electric current density, which flows **parallel to the rim** of the PEC half plane

Scalar Nature of the Problem

The problem can thus be reduced to a **scalar one** in terms of the scattered electric field.

By letting $\mathcal{D} = \{z = 0, x \geq 0\}$ be the PEC half plane, we have:

$$\nabla_{xz}^2 E_y^s + k_0^2 E_y^s = 0, \text{ in } \mathbb{R}_{xz}^2 \setminus \mathcal{D}$$

2D Helmholtz equation

$$E_y^s = -E_y^i = -E_0^i e^{-jk_0 \sin \theta^i x}, \text{ on } \mathcal{D}$$

boundary condition
on the PEC half plane

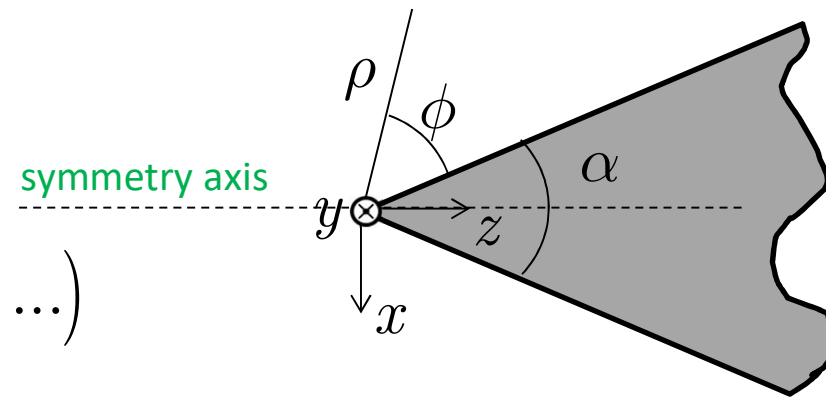
Edge Condition

To ensure the uniqueness of the solution, the correct behavior of the field quantities in the vicinity of the **geometrical singularities** (edges, vertices) of the boundary must be specified.

Consider for instance a PEC wedge with internal angle α placed inside a uniform dielectric medium:

$$E_y \sim \rho^\nu (a_0 + a_1 \rho + \dots)$$

$$\Rightarrow H_x, H_z \sim \rho^{\nu-1} (b_0 + b_1 \rho + \dots)$$



Generally, the behavior of an electromagnetic field in the neighborhood of the common edge of angular dielectric or conducting regions is determined from the condition that **the energy density must be integrable over any finite domain** (the so-called **edge condition**).

[J. Meixner, "Die Kantenbedingung in der Theorie der Beugung elektromagnetischer Wellen an vollkommen leitenden ebenen Schirmen," *Ann. Phys.*, vol. 6, pp. 1-9, 1949.]

Edge Condition

By further enforcing the boundary conditions on the faces of the PEC wedge, the exponent ν can be determined as

$$\nu = \frac{\pi}{2\pi - \alpha}$$

Therefore, in the case of a PEC half plane, equivalent to a PEC wedge with zero internal angle, it results $\nu = 1/2$:

$$E_y \sim \rho^{1/2}$$

$$H_x, H_z, J_z \sim \rho^{-1/2}$$

$$\rho = \sqrt{x^2 + z^2} \rightarrow 0$$

Symmetry of the Scattered Field

- The scattered field is produced by the current density on the PEC half plane, which is purely tangential.
- The plane $z = 0$ is a symmetry plane for the scattered field.



The scattered field is **even-symmetric** w.r.t. the $z=0$ plane:

$$E_y^s(x, -z) = E_y^s(x, z)$$

hence it is sufficient to find the scattered field in the half space $z \geq 0$

Diffraction = Interaction + Propagation

As any problem of diffraction by a screen, also the present one can be decomposed into two steps:

1) Interaction problem

Find the scattered field on the plane $z = 0$. In the present case, since the scattered field is known on the PEC half plane, this reduces to determining the scattered field on the half plane $z = 0, x < 0$.

2) Propagation Problem

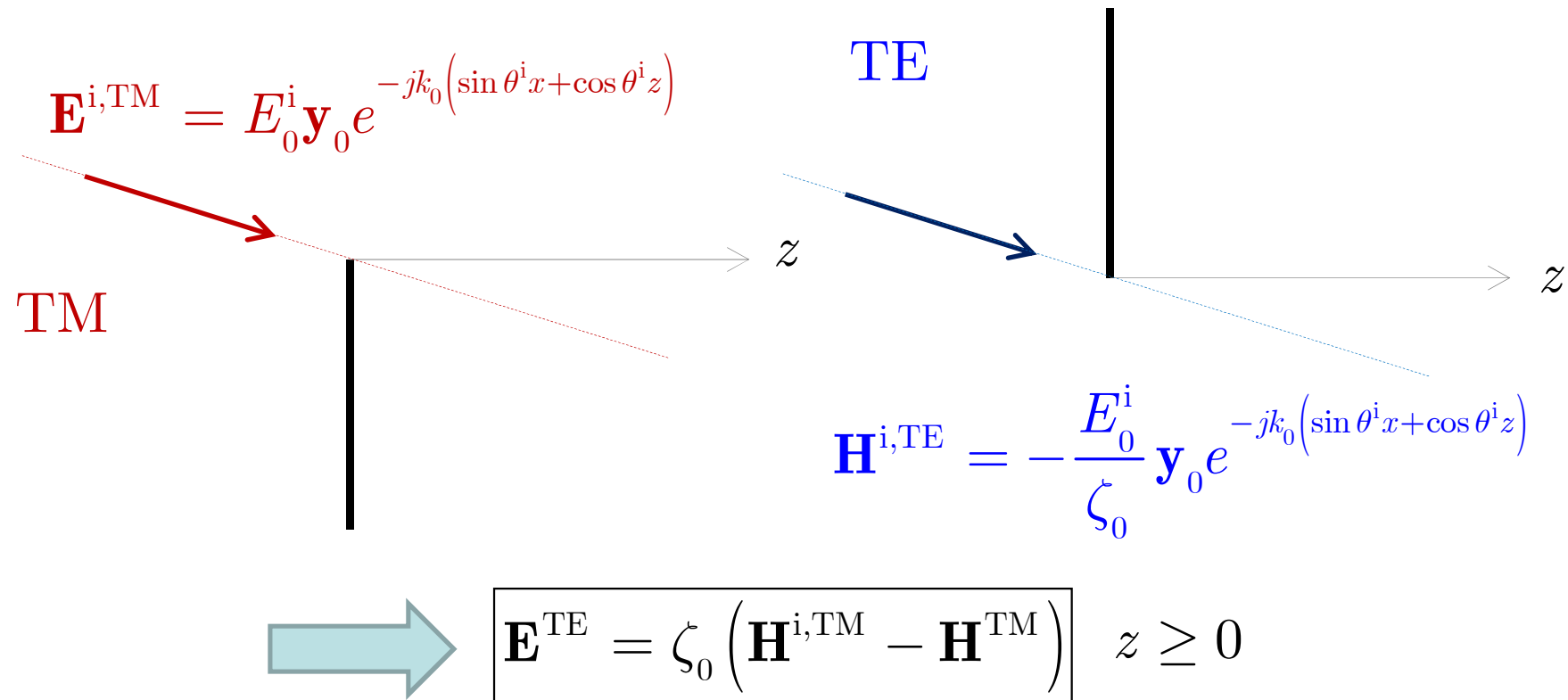
Determine the field in the half space $z > 0$ from knowledge of the field on the plane $z = 0$ (the so-called 'aperture field')

Note: the difficult part is 1); in fact, 2) can be solved by expressing the field in the half space $z > 0$ through standard radiation integrals in terms of the aperture field.

Generalizations: TE Incidence

It is important to observe that, once a solution has been found, it can be immediately generalized in different directions.

First, the case of TE incidence can be obtained by using the **Babinet principle** in its full electromagnetic form:



Generalizations: Oblique Incidence

Let us now consider an incident plane wave propagating at an angle ψ^i w.r.t. the y axis:

$$\mathbf{E}^{i,\text{TM}} = \mathbf{y}_0 e^{-jk_0 \cos \psi^i y} \underbrace{e^{-jk_0 \sin \psi^i (\sin \theta^i x + \cos \theta^i z)}}_{\doteq e_y^i(x, z; k_0, \psi^i, \theta^i)}$$

(the case of normal incidence being recovered by letting $\psi^i = \pi/2$).

Since this is an **eigenfunction** of any **translation operator** along the y axis and since the structure is **translationally invariant** along the same axis, we conclude that the scattered field must be of the form:

$$\mathbf{E}^{s,\text{TM}} = \mathbf{y}_0 e^{-jk_0 \cos \psi^i y} e_y^s(x, z; k_0, \psi^i, \theta^i)$$

Generalizations: Oblique Incidence

normal incidence

$$\nabla_{xz}^2 e_y^s + k_0^2 e_y^s = 0, \text{ in } \mathbb{R}_{xz}^2 \setminus \mathcal{D}$$

$$e_y^s = -E_0^i e^{-jk_0 \sin \theta^i x}, \text{ on } \mathcal{D}$$

oblique incidence

$$\nabla_{xz}^2 e_y^s + k_t^2 e_y^s = 0, \text{ in } \mathbb{R}_{xz}^2 \setminus \mathcal{D}$$

$$e_y^s = -E_0^i e^{-jk_t \sin \theta^i x}, \text{ on } \mathcal{D}$$

$$k_t = k_0 \sin \psi^i$$



$$e_y^s(x, z; k_0, \psi^i, \theta^i) = e_y^s\left(x, z; k'_0 = k_0 \sin \psi^i, \frac{\pi}{2}, \theta^i\right)$$

The scattered field for oblique incidence can be obtained from the scattered field for normal incidence calculated at the **scaled frequency** $\omega' = \omega \sin \psi^i$

The Sommerfeld Half-Plane Problem: Elementary Solution

Cylindrical Waves of Half-Integer Order

The interaction problem can be solved using a superposition of **elementary solutions of the Helmholtz equation** which correspond to fields that could be generated by currents flowing only in the half plane $x \geq 0, z = 0$.

[F. Gori, "Diffraction from a half plane. A new derivation of the Sommerfeld solution," *Optics Commun.*, vol. 48, no. 2, pp. 67–70, Nov. 1983.]

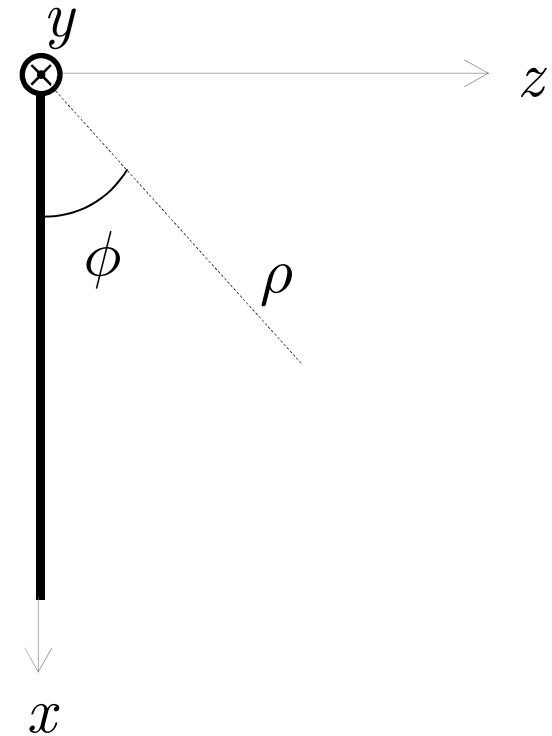
Consider the electric field

$$E_y = E_0 \frac{e^{-jk_0\rho}}{\sqrt{k_0\rho}} \sin\left(\frac{\phi}{2}\right)$$

$\underbrace{\hspace{10em}}_{\text{with } 0 \leq \phi \leq 2\pi} = \sqrt{\frac{\pi}{2}} H_{1/2}(k_0\rho)$

with $0 \leq \phi \leq 2\pi$

This is the electric field of an **anisotropic cylindrical wave** of order $n = 1/2$.

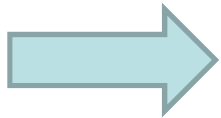


Cylindrical Waves of Half-Integer Order

The relevant magnetic field is:

$$\mathbf{H} = -\frac{1}{j\omega\mu_0} \nabla \times \mathbf{E} = -\frac{1}{jk_0\zeta_0} \left[\rho_0 \frac{1}{\rho} \frac{\partial E_y}{\partial \phi} - \phi_0 \frac{\partial E_y}{\partial \rho} \right]$$

$$H_\rho = j \frac{E_0}{\zeta_0} \frac{e^{-jk_0\rho}}{(k_0\rho)^{3/2}} \frac{1}{2} \cos\left(\frac{\phi}{2}\right) \quad \text{discontinuous on } \phi = 0, 2\pi$$



$$H_\phi = -j \frac{E_0}{\zeta_0} \frac{1 + 2jk_0\rho}{(k_0\rho)^{3/2}} e^{-jk_0\rho} \frac{1}{2} \sin\left(\frac{\phi}{2}\right) \quad \text{continuous everywhere}$$

Cylindrical Waves of Half-Integer Order

We deduce that the field of this cylindrical wave is produced by a y -directed surface current which is **nonzero only on the half plane** $\phi = 0$:

$$J_y = \left[H_\rho \right]_{\phi=2\pi}^{\phi=0} = j \frac{E_0}{\zeta_0} \frac{e^{-jk_0\rho}}{(k_0\rho)^{3/2}}, \quad \text{on } \phi = 0$$

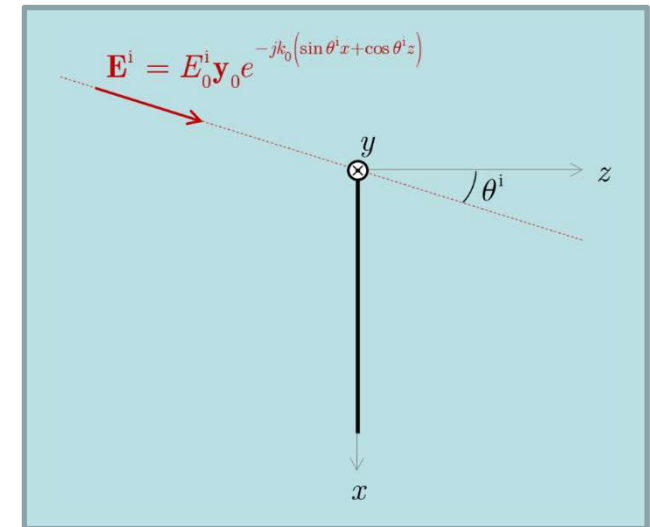
In order to solve the interaction problem, we will look for a **superposition** of such cylindrical waves, with their axes (parallel to one another and to the y -plane) lying on the half-plane $x \geq 0, z = 0$.

Enforcing the Boundary Condition

Since E_y vanishes for $\phi = 0$, the electric field at any point on the x -axis depends only on the waves originating on the right of that point.


Therefore, we may write:

$$E_y^s(x, z = 0) = \int_x^{+\infty} p(\xi) \frac{e^{-jk_0(\xi-x)}}{\sqrt{k_0(\xi-x)}} d\xi, \quad x \geq 0$$



The function $p(\xi)$ must be such that the scattered field be equal and opposite to the incident field for any $x \geq 0$. This allows us for obtaining an integral equation with the function $p(\xi)$ as an unknown...

Enforcing the Boundary Condition


$$\int_x^{+\infty} p(\xi) \frac{e^{-jk_0(\xi-x)}}{\sqrt{k_0(\xi-x)}} d\xi = -E_0^i e^{-jk_0 \sin \theta^i x}, \quad x \geq 0$$

By a simple change of variable we have:

$$\int_0^{+\infty} p(\xi' + x) \frac{e^{-jk_0 \xi'}}{\sqrt{k_0 \xi'}} d\xi' = -E_0^i e^{-jk_0 \sin \theta^i x}, \quad x \geq 0$$

whose solution is found by inspection to simply be an **exponential function**:

$$p(\xi) = -CE_0^i e^{-jk_0 \sin \theta^i \xi} \Rightarrow p(\xi' + x) = -CE_0^i e^{-jk_0 \sin \theta^i x} e^{-jk_0 \sin \theta^i \xi'}$$


Enforcing the Boundary Condition

By inserting this into the equation, we may find the value of the constant C :

$$C \int_0^{+\infty} e^{-jk_0 \sin \theta^i \xi'} \frac{e^{-jk_0 \xi'}}{\sqrt{k_0 \xi'}} d\xi' = 1$$

whence, by letting $\mu^2 = k_0 \xi' (1 + \sin \theta^i)$

$$\frac{2C}{k_0 \sqrt{1 + \sin \theta^i}} \underbrace{\int_0^{+\infty} e^{-j\mu^2} d\mu}_{= e^{-j\pi/4} \sqrt{\pi}/2} = 1 \quad \text{(complete Fresnel integral)}$$


$$C = \frac{k_0}{\sqrt{\pi}} e^{+j\pi/4} \sqrt{1 + \sin \theta^i}$$

Solution of the Interaction Problem

The scattered field on the entire aperture plane $z = 0$ is finally

$$E_y^s(x, z = 0) = \begin{cases} -E_0^i e^{-jk_0 \sin \theta^i x}, & x \geq 0 \\ -\frac{2E_0^i}{\sqrt{\pi}} e^{+j\pi/4} F\left(\sqrt{k_0 |x| (1 + \sin \theta^i)}\right), & x < 0 \end{cases}$$

where

$$F(t) = \int_t^{+\infty} e^{-j\mu^2} d\mu$$

is a complex Fresnel integral.

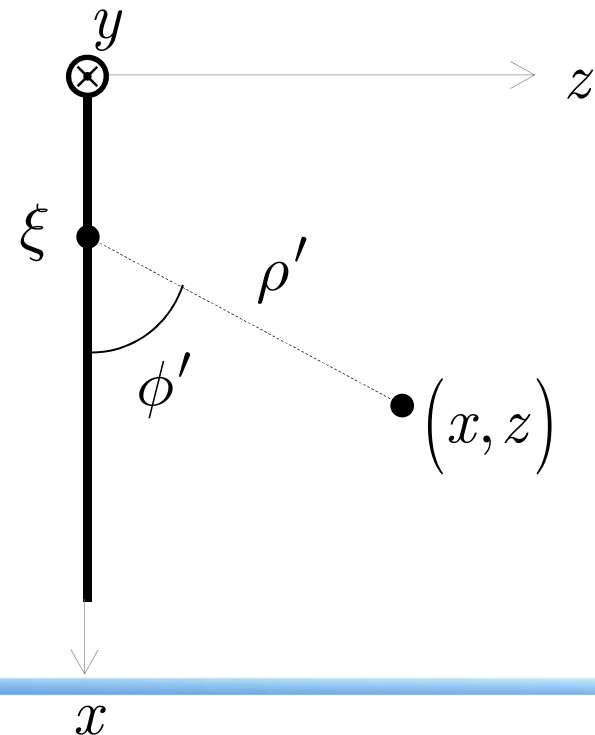
Solution of the Propagation Problem

The scattered field in the half space $z > 0$ can be calculated with any propagation formula like the Rayleigh-Sommerfeld or the plane-wave expansion formulas.

Alternatively, the scattered field at any point can be evaluated directly as a superposition of the half-integer cylindrical waves employed to solve the interaction problem:

$$E_y^s(x, z \geq 0) = \int_0^{+\infty} p(\xi) \frac{e^{-jk_0 \rho'}}{\sqrt{k_0 \rho'}} \sin \frac{\phi'}{2} d\xi$$

$$\rho' = \sqrt{(x - \xi)^2 + z^2} \quad \tan \phi' = \frac{z}{x - \xi}$$

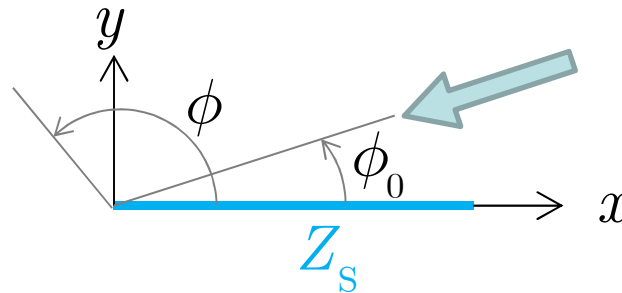


**The Sommerfeld Half-Plane Problem:
Dual Integral Equations/Wiener-Hopf Method**

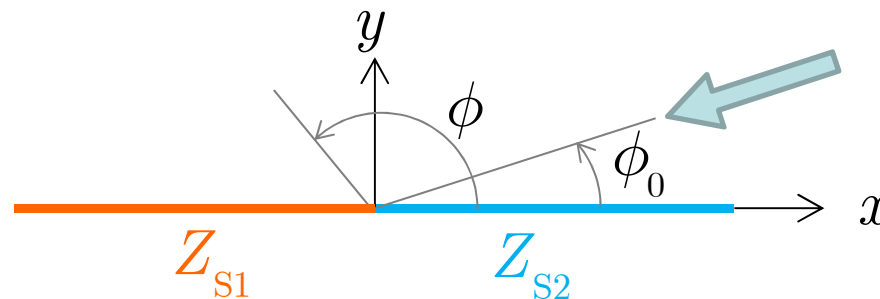
The Wiener-Hopf Method

The analysis of the half-plane diffraction problem is generally carried out with the **Wiener-Hopf method**, which allows for generalizing the solution to

- **half planes with impedance boundary/transition conditions:**



- **two-part impedance planes:**



The Wiener-Hopf Method

The analytical solution of the integral equation that results from the application of the boundary conditions is obtained in the Wiener-Hopf method by:

- 1) **taking the Fourier transform** of the integral equation, thereby
- 2) **reducing it to a functional equation**, which is in turn solved by invoking properties of analytic functions (crucially, the generalized *Liouville theorem* for entire functions).

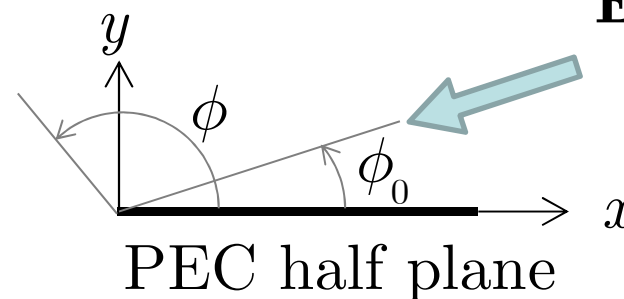
[\[https://en.wikipedia.org/wiki/Liouville%27s_theorem_\(complex_analysis\)\]](https://en.wikipedia.org/wiki/Liouville%27s_theorem_(complex_analysis))

Since the crucial (and most difficult) step of the method consists in **factorizing** a given function into the product of **functions analytic (and without zeroes) in the upper and lower halves of the complex plane**, the method is also known (especially in the Soviet literature) as the **Factorization Method**.

Wiener-Hopf Method vs. Dual Integral Equations

A mathematically equivalent but more direct approach, that works directly with the spectra of the field quantities, was proposed in 1951 by Clemmow and is based on the so-called **dual integral equations**.

Since this requires fewer steps to arrive at the solution, it will be adopted here to illustrate the solution for the case of a PEC half plane, TM polarization:


$$\mathbf{E}^{i, \text{TM}} = E_0^i \mathbf{z}_0 e^{jk_0 \rho \cos(\phi - \phi_0)}$$

[T. B. A. Senior and J. L. Volakis, *Approximate boundary conditions in electromagnetics*. London, UK: The IEE, 1995, ch. 3.]

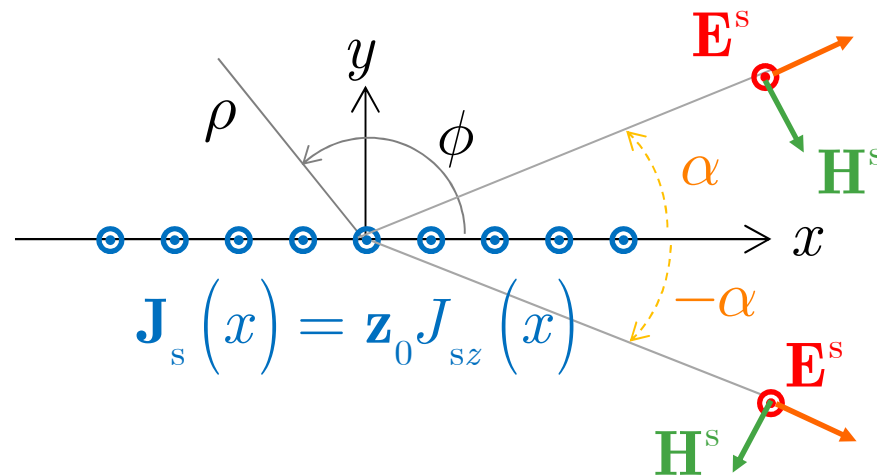
Angular Spectrum Representation of the Fields

A key feature of the dual-integral-equation method is the *a-priori* introduction of the **angular spectrum** $P_e(\cos\alpha)$ of the scattered field:

$$E_z^s(\rho, \phi) = E_0^i \int_c^c P_e(\cos\alpha) e^{-jk_0\rho \cos(\phi \pm \alpha)} d\alpha, \quad y \geq 0$$

$$H_x^s(\rho, \phi) = \pm \frac{E_0^i}{\zeta_0} \int_c^c \sin\alpha P_e(\cos\alpha) e^{-jk_0\rho \cos(\phi \pm \alpha)} d\alpha, \quad y \geq 0$$

valid for fields due to a z -directed electric current distribution in the $y = 0$ plane:



Angular Spectrum Representation of the Fields

To prove the validity of the angular-spectrum representation let us consider the field radiated by the surface current:

$$E_z^s(x, y) = -j\omega\mu_0 \int_{-\infty}^{+\infty} J_{sz}(x') \frac{1}{4j} H_0^{(2)} \left(k_0 \sqrt{(x-x')^2 + y^2} \right) dx'$$

(Green's function for the 2D scalar Helmholtz equation)

By letting $y = 0$:

$$\begin{aligned} E_z^s(x, 0) &= -j\omega\mu_0 \int_{-\infty}^{+\infty} J_{sz}(x') \frac{1}{4j} H_0^{(2)}(k_0 |x-x'|) dx' \\ &= -j\omega\mu_0 J_{sz}(x) \otimes \frac{1}{4j} H_0^{(2)}(k_0 |x|) \end{aligned}$$

Angular Spectrum Representation of the Fields

By Fourier-transforming w.r.t. x : $\tilde{E}_z^s(k_x, 0) = -j\omega\mu_0 \tilde{J}_{sz}(k_x) \frac{1}{2jk_y}$

where $k_y = \begin{cases} \sqrt{k_0^2 - k_x^2}, & k_x \leq k_0 \\ -j\sqrt{k_x^2 - k_0^2}, & k_x \geq k_0 \end{cases}$

hence

$$\tilde{E}_z^s(k_x, y) = -j\omega\mu_0 \tilde{J}_{sz}(k_x) \frac{e^{-jk_y|y|}}{2jk_y}$$

and finally, by inverse Fourier-transforming:

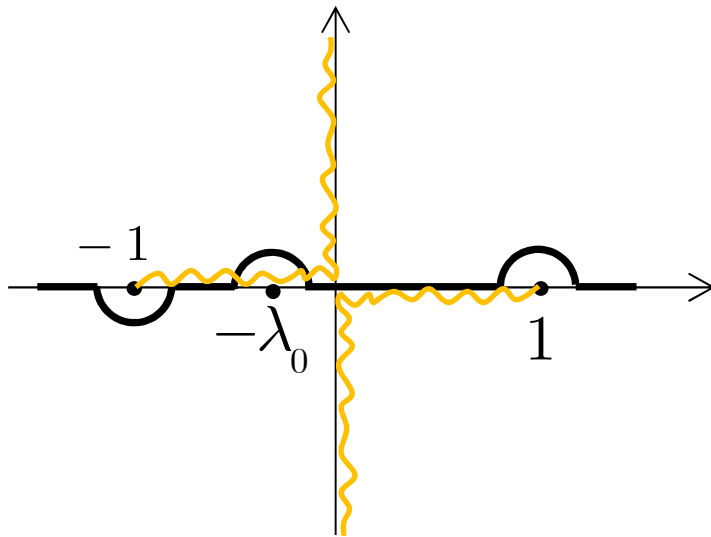
$$E_z^s(x, y) = -\frac{\omega\mu_0}{4\pi} \int_{-\infty}^{+\infty} \tilde{J}_{sz}(k_x) \frac{e^{-jk_y|y|}}{k_y} e^{-jk_x x} dk_x$$

Angular Spectrum Representation of the Fields

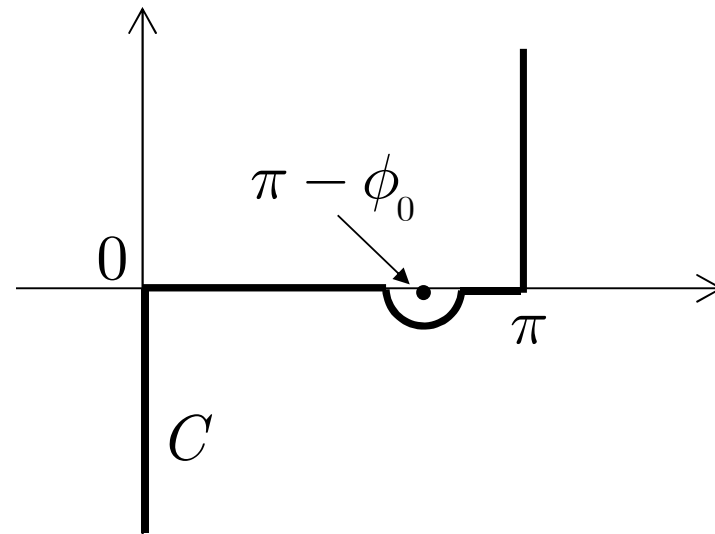
We now make the change of variable:

$$k_x = k_0 \lambda = k_0 \cos \alpha,$$

$$k_y = k_0 \sqrt{1 - \lambda^2} = k_0 \sin \alpha$$



complex λ -plane



complex α -plane

(the origin and meaning of the indicated pole will be clarified in subsequent slides)

Angular Spectrum Representation of the Fields

This leads to the postulated angular-spectrum representation:

$$E_z^s(x, y) = -\frac{\omega\mu_0}{4\pi} \int_C \tilde{J}_{sz}(k_0 \cos \alpha) e^{-jk_0(x \cos \alpha + |y| \sin \alpha)} d\alpha$$

$$E_z^s(\rho, \phi) = \int_C \underbrace{-\frac{\omega\mu_0}{4\pi} \tilde{J}_{sz}(k_0 \cos \alpha)}_{=E_0^i P_e(\cos \alpha)} e^{-jk_0 \rho \cos(\phi \mp \alpha)} d\alpha, \quad y \geq 0$$



$$H_x^s(\rho, \phi) = \pm \frac{E_0^i}{\zeta_0} \int_C \sin \alpha P_e(\cos \alpha) e^{-jk_0 \rho \cos(\phi \mp \alpha)} d\alpha, \quad y \geq 0$$

Spectral Representation of the Fields

Alternatively, using the normalized spectral variable λ , we have the spectral representation of the fields:

$$E_z^s(x, y) = E_0^i \int_{-\infty}^{+\infty} \frac{P_e(\lambda)}{\sqrt{1-\lambda^2}} e^{-jk_0 x \lambda} e^{-jk_0 |y| \sqrt{1-\lambda^2}} d\lambda$$

$$H_x^s(x, y) = \pm \frac{E_0^i}{\zeta_0} \int_{-\infty}^{+\infty} P_e(\lambda) e^{-jk_0 x \lambda} e^{-jk_0 |y| \sqrt{1-\lambda^2}} d\lambda$$

Boundary Condition for the Electric Field

Let us write the electric field on the plane $y = 0$ using the λ variable:

$$E_z^s(x, y = 0) = E_0^i \int_{-\infty}^{+\infty} \frac{P_e(\lambda)}{\sqrt{1 - \lambda^2}} e^{-jk_0 x \lambda} d\lambda$$

The boundary condition on the PEC plane is: $E_z^s(x, y = 0) + E_z^i(x, y = 0) = 0$



$$\int_{-\infty}^{+\infty} \frac{P_e(\lambda)}{\sqrt{1 - \lambda^2}} e^{-jk_0 x \lambda} d\lambda = -e^{jk_0 x \cos \phi_0}, \quad x > 0$$

Boundary Condition for the Magnetic Field

From the spectral representation of the magnetic field we find that it is an **odd function** of y (as expected, by symmetry). In particular, on the plane $y = 0$ we have:

$$H_x^s(x, y = 0^+) = \frac{E_0^i}{\zeta_0} \int_{-\infty}^{+\infty} P_e(\lambda) e^{-jk_0 x \lambda} d\lambda = -H_x^s(x, y = 0^-)$$

On the other hand, from the boundary condition for the magnetic field:

$$H_x^s(x, y = 0^+) - H_x^s(x, y = 0^-) = -J_{sz}(x)$$

and the fact that the electric current density exists only on $y = 0, x > 0$:

$$H_x^s(x, y = 0^+) = H_x^s(x, y = 0^-), \quad x < 0$$



$$\int_{-\infty}^{+\infty} P_e(\lambda) e^{-jk_0 x \lambda} d\lambda = 0, \quad x < 0$$

Support of the Electric Current Density

We may arrive at the same integral equation by recalling that the spectrum $P_e(\lambda)$ is proportional to the spectral electric surface current density:

$$P_e(\lambda) = -\frac{\omega\mu_0}{4\pi E_0^i} \tilde{J}_{sz}(k_0\lambda)$$

hence by inverse Fourier-transforming:

$$J_{sz}(x) = -\frac{2E_0^i}{\omega\mu_0} \int_{-\infty}^{+\infty} P_e(\lambda) e^{-jk_0x\lambda} d\lambda$$

and, since the electric current density is nonzero only on the PEC half plane $y = 0, x > 0$, we again find:

$$\int_{-\infty}^{+\infty} P_e(\lambda) e^{-jk_0x\lambda} d\lambda = 0, \quad x < 0$$

Dual Integral Equations

Let us collect the two equations thus obtained:

$$\int_{-\infty}^{+\infty} \frac{P_e(\lambda)}{\sqrt{1-\lambda^2}} e^{-jk_0 x \lambda} d\lambda = -e^{jk_0 x \cos \phi_0}, \quad x > 0$$

$$\int_{-\infty}^{+\infty} P_e(\lambda) e^{-jk_0 x \lambda} d\lambda = 0, \quad x < 0$$

Integral equations of this kind, sharing the **same unknown** but having **different kernels** and **different domains of validity** (in this case, the half lines $x < 0$, $x > 0$) are commonly referred to as **dual integral equations**.

In what follows, they will be solved analytically by means of complex analysis...

Analiticity of the Spectrum in the Upper Plane

Let us recall the connection of the spectrum $P_e(\lambda)$ to the spectral electric current density:

$$\begin{aligned} P_e(\lambda) &= -\frac{\omega\mu_0}{4\pi E_0^i} \tilde{J}_{sz}(k_0\lambda) = -\frac{\omega\mu_0}{4\pi E_0^i} \int_{-\infty}^{+\infty} J_{sz}(x) e^{+jk_0x\lambda} dx \\ &= -\frac{\omega\mu_0}{4\pi E_0^i} \int_0^{+\infty} J_{sz}(x) e^{+jk_0x\lambda} dx \end{aligned}$$

and let us integrate this along an **arbitrary closed contour** Γ in the upper λ -plane:

$$\oint_{\Gamma} P_e(\lambda) d\lambda = -\frac{\omega\mu_0}{4\pi E_0^i} \oint_{\Gamma} \int_0^{+\infty} J_{sz}(x) e^{+jk_0x\lambda} dx d\lambda$$

Thanks to the fact that the inner integral is esponentially convergent at infinity when λ is in the upper half plane, we can invoke the Fubini-Tonelli theorem and **change the order of integrations**:

Analiticity of the Spectrum in the Upper Plane

$$\Rightarrow \oint_{\Gamma} P_e(\lambda) d\lambda = -\frac{\omega\mu_0}{4\pi E_0^i} \int_0^{+\infty} J_{sz}(x) \underbrace{\oint_{\Gamma} e^{+jk_0 x \lambda} d\lambda}_{=0} dx = 0$$

We can now make use of **Morera's theorem** to deduce that **the spectrum is analytic in the upper half plane**.

We will indicate this by setting it equal to an (unknown) "upper" half-plane function, namely:

$$P_e(\lambda) = U(\lambda)$$

(note that this is only a temporary change in the name of the function P_e)

Closing the Contour at Infinity

Note that, by closing the integration path by an infinite semicircular contour in the **upper half plane** (which is possible when $x < 0$), the analyticity of the spectrum and Cauchy's Theorem allow for concluding that **the second integral equation is satisfied**, i.e.,

$$\int_{-\infty}^{+\infty} U(\lambda) e^{-jk_0 x \lambda} d\lambda = 0, \quad x < 0$$

In order to solve the other integral equation, i.e.,

$$\int_{-\infty}^{+\infty} \frac{U(\lambda)}{\sqrt{1-\lambda^2}} e^{-jk_0 x \lambda} d\lambda = -e^{jk_0 x \cos \phi_0}, \quad x > 0$$

we will again close the integration path by an infinite semicircular contour, but this time in the **lower half plane**, since $x > 0$.

Closing the Contour at Infinity

To recover the right hand side of the latter integral equation by means of the **Residue Theorem** we write the integrand in the form

$$\frac{U(\lambda)}{\sqrt{1-\lambda^2}} = \frac{1}{2\pi j} \frac{L_1(\lambda)}{L_1(-\lambda_0)} \frac{1}{\lambda + \lambda_0} + L_2(\lambda)$$

where $L_{1,2}(\lambda)$ are unknown "lower" functions (i.e., functions analytic in the lower half λ -plane) and

$$\lambda_0 = \cos \phi_0 \quad (\text{'optical pole'})$$

Despite the presence of three unknown functions, the above **functional equation** is sufficient to determine $U(\lambda)$...

Splitting Procedure

The standard approach is to decompose all functions into functions that are analytic as well free of zeros in either the upper or lower half-plane.

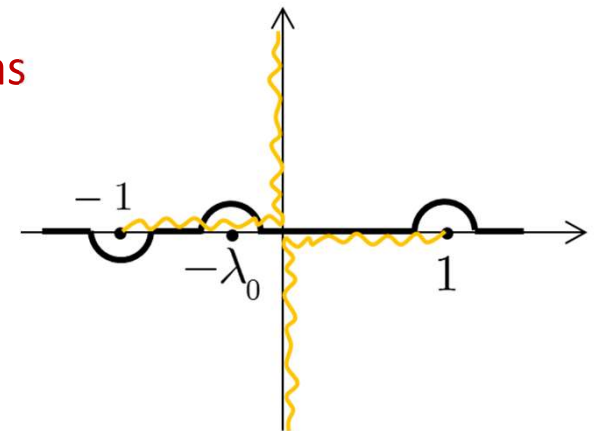
This procedure is commonly referred to as the **factorization** or **splitting** of a complex function as

$$F(\lambda) = F_+(\lambda)F_-(\lambda)$$

where $F_+(\lambda)$ is the "upper split" function and $F_-(\lambda)$ is the "lower split" function.

In this case, the function $\sqrt{1 - \lambda^2}$ can be decomposed as

$$K(\lambda) = \sqrt{1 - \lambda^2} = \underbrace{\sqrt{1 - \lambda}}_{K_+(\lambda)} \underbrace{\sqrt{1 + \lambda}}_{K_-(\lambda)}$$



complex λ -plane

Separating the Upper and Lower Functions

By inserting the split form into the functional equation we have:

$$\frac{U(\lambda)}{K_+(\lambda)} = \frac{1}{2\pi j} \frac{L_1(\lambda)}{L_1(-\lambda_0)} \frac{K_-(\lambda)}{\lambda + \lambda_0} + K_-(\lambda) L_2(\lambda)$$

In order to remove the optical pole (which lies in the lower half plane) from the right-hand side we may rewrite the previous equation as

$$\frac{U(\lambda)}{K_+(\lambda)} - \frac{1}{2\pi j} \frac{K_+(\lambda_0)}{\lambda + \lambda_0} = \frac{1}{2\pi j} \left[\frac{L_1(\lambda)}{L_1(-\lambda_0)} \underbrace{K_-(\lambda)}_{=K_+(-\lambda)} - K_+(\lambda_0) \right] \frac{1}{\lambda + \lambda_0} + K_-(\lambda) L_2(\lambda)$$

so that now the left hand side is an "upper function", whereas the right hand side is a "lower function"...

Behavior at Infinity

From the edge condition for the surface current density and **Watson's lemma** we have

$$J_z \underset{x \rightarrow 0}{\sim} x^{-1/2} \quad \Rightarrow \quad U(\lambda) = P_e(\lambda) \propto \tilde{J}_z(k_0 \lambda) \underset{\lambda \rightarrow \infty}{\sim} \lambda^{-1/2}$$

We deduce that the left hand side of the modified functional equation is **infinitesimal at infinity** (with order λ^{-1}):

$$\frac{\underset{\sim \lambda^{-1/2}}{U(\lambda)}}{\underset{\sim \lambda^{1/2}}{K_+(\lambda)}} - \frac{1}{2\pi j} \frac{K_+(\lambda_0)}{\lambda + \lambda_0} \sim \lambda^{-1}$$

The Crucial Step

- Since the left and right hand sides of the modified functional equations are upper and lower functions, respectively, they must both be **entire functions**.
- Furthermore, since they are infinitesimal at infinity, they are **bounded entire functions** and hence, by **Liouville Theorem**, they must be equal to a **constant**.
- Finally, since they are infinitesimal at infinity, such a constant must be **equal to zero**:

$$\frac{U(\lambda)}{K_+(\lambda)} - \frac{1}{2\pi j} \frac{K_+(\lambda_0)}{\lambda + \lambda_0} = 0$$

The Solution for the Angular Spectrum

Hence

$$P_e(\lambda) = U(\lambda) = \frac{1}{2\pi j} \frac{K_+(\lambda) K_+(\lambda_0)}{\lambda + \lambda_0} = \frac{1}{2\pi j} \frac{\sqrt{1-\lambda} \sqrt{1-\lambda_0}}{\lambda + \lambda_0}$$

or

$$P_e(\cos \alpha) = \frac{1}{2\pi j} \frac{\sqrt{1-\cos \alpha} \sqrt{1-\cos \phi_0}}{\cos \alpha + \cos \phi_0}$$

The angular spectrum of the scattered field has thus been found in a **closed analytical form**.

References

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